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SIMPLE DESIGN OF CO-POLARIZATION BROADBAND METAMATERIAL ABSORBER FOR C-BAND APPICATIONS

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ABSTRACT

imple design of a novel co-polarization wideband metamaterial absorber (MA) for C-band cations is proposed and numerical investigated. The unit cell of the proposed MA is designed by bining the haft-moon shaped resonator (HMSR) and interior circle resonator (ICR) structures, based substrate. The absorption performances of the proposed absorber are numerical investigated. The cosed absorber achieves the co-polarization absorptivity higher than 90% covering the entire C-band 3.95 GHz to 8.02 GHz under normal incidence for transverse electric (TE) and transverse magnetic polarizations. Moreover, the average absorption can be maintained above 80% even for incident up to 600 under both TE and TM polarizations. The physical mechanism of the proposed MA is designed by using the electric and surface current distributions, which is also supported by the electromagnetic parameters. The design in this work is a compact structure (unit cell insensitivity, which can be applications in the C-band defense and stealth systems.

INTRODUCTION

Metamaterial absorber (MA) has attracted derable interest in both fundamental earch and device applications, since Landy et seported a thin perfect microwave MA based electric and magnetic resonances in 2008 [1-Bowever, the realizing MA structures having le design, thin thickness, easy fabrication and broadband absorption features for applications in microwave range such and ar cross section reduction (RSC), stealth interference (EMI) and EM mology challenging. truly remains broadband the design mermore, wave MAs have been mostly focused on sequency band above C-band, but very few of MA for lower frequency absorption such as C-band, has been reported [2,4]. this paper, we propose a simple design of co-polarization wideband metamaterial mer (MA) for C-band applications. The unit of the proposed MA is designed by ning the haft-moon shaped resonator and interior circle resonator (ICR) based on FR4 substrate.

EXPERIMENTAL

Fig. 1 shows the unit cell of the proposed broadband MA. The broadband MA is formed by the periodic arrangement of the unit cells in the lateral directions and the vertical thickness consists of two metallic films separated by a dielectric layer. The metallic layers are made of copper with an electric conductivity of and thickness (t) of 0.035 mm. The dielectric layer is made of FR4 with a relative dielectric constant of 4.3, a loss - tangent of 0.025, and thickness (h) of 4.2 mm. The front layer is constituted by the combination of haft-moon shaped resonator (HMSR) and interior circle resonator (ICR) structure. The geometrical dimensions of the unit cell are R₁=6.3 mm, R₂=3.35 mm, r=3.65 mm, and a=15.4 mm. The center of the circles with radii R₁ and R₂ are O₁(0,0) and O₂(1.775,-1.175), respectively. For back layer of the structure, copper is used in order to block all transmission.

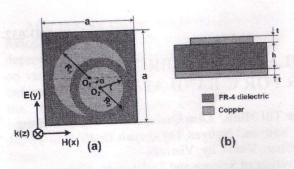


Figure 1. A unit cell geometry of the proposed MA: (a) top-view and (b) side-view.

In order to investigate the absorption performance of the proposed MA, the numerical simulation is performed by using frequency domain solver in a Computer Simulation Technology (CST) Microwave Studio. In the boundary condition set up, z-direction and x-y plane are for the direction of propagation and the E-H fields, x and y axes are fixed to the unit cell and z axis is open, the plane waves are normally incident to the structure along the z direction.

The absorption is defined by $A(\omega) = 1 - T(\omega) - R(\omega)$, where $T(\omega)$ and $R(\omega)$ are transmission and reflection, respectively. The $A(\omega)$ and $T(\omega)$ are determined from the frequency-dependent S-parameters $S_{11}(\omega)$ and $S_{21}(\omega)$, where $T(\omega) = |S_{21}(\omega)|^2$ and $R(\omega) = |S_{11}(\omega)|^2$. The reflection is calculated as $R(\omega) = |r_{yy}(\omega)|^2 + |r_{xy}(\omega)|^2$, where $r_{yy}(\omega) = |E_{yr}|^2 / |E_{yi}|^2$ and $r_{xy}(\omega) = |E_{xr}|^2 / |E_{yi}|^2$ are reflection coefficients for co-polarization and cross-polarization for y (or TE) polarized wave, respectively. In the conventional absorber model, the back layer acts as physical barrier to block the transmittance. Since $T(\omega)$ is eliminated by the ground plane, thus, the absorption is simplified to $A(\omega) = 1 - R(\omega)$.

RESULTS AND DISCUSSION

The absorption performances of the proposed absorber are numerical investigated. The proposed absorber achieves the copolarization absorptivity higher than 90% covering the entire C-band from 3.95 GHz to 8.02 GHz under normal incidence as seen in Fig.2. Moreover, the average absorption can be maintained above 80% even for incident angles up to 60° under both TE and TM polarizations.

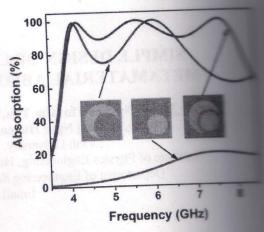


Figure 2. Absorption spectra of two composed of the combined proposed MA structure.

To investigate the mechanism absorbed the proposed MA, the distributions of field and surface current at three frequencies of 4.19 GHz, 5.63 GHz, are performed as shown in Fig. 3.

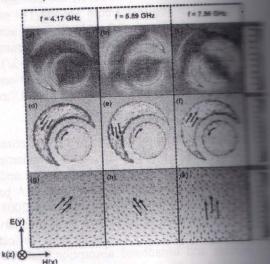


Figure 3. Distributions of (a),(b),(c) field, and surface current on (d),(e),(f) the layer and (g),(h),(k) back layer of a under TE polarization with various frequencies of 4.19 GHz, 5.63 GHz, and GHz, respectively.

It can be seen from Figs. 3(a-c), the field with a specified frequency is concernate at a certain part of MA. At lower frequence 4.19 GHz and 5.63 GHz, electric field accumulate at inner top and bottom part HMSR, respectively. Meanwhile, at frequency of 7.58 GHz, the electric field concentrated not only the outer of ICR but also in inner the top and bottom part of the concentrated part of the

The top and bottom surface current are illustrated in Figs. 3(d-k). At resonance frequencies, the surface mainly contributed by HMSR, while amount of current flows through higher frequency of 7.58 GHz. At the of 7.58 GHz, the surface currents on and the HMSR are anti-parallel to that bottom layer. This means the peak at the bequency is not only mainly contributed magnetic resonance of the ICR, but also weak anti-parallel currents between the HMSR. However, at the lower frequencies of 4.19 GHz and 5.63 surface currents are strong coupled edges of HMRS. Thus, the strong electric field is created and it reverses to dent electric field, which confirms the electric field is stronger than the incident field. It is clear that the electric excited at 4.19 GHz and 5.63 GHz. time, the surface current distribution HMSR is anti-parallel with the current in the ground layer, thus the current is created and formed the magnetic field. The induced magnetic reverse with incident magnetic field, that the strong magnetic resonance is matributed in these resonant frequencies. both the magnetic and the electric are excited simultaneously at the requencies of 4.19 GHz and 5.63 GHz.

CONCLUSION

simple design of a novel co-polarization MA based on asymmetric structure is and investigated using numerical The unit cell of the proposed structure of metallic shape created by the ation of HMSR and ICR structure and plane separated by a dielectric layer. The of the structural parameters on the coreation absorption is thoroughly gated. The proposed MA shows a coabsorptivity of higher than 90% in handwidth from 3.95 GHz to 8.02 GHz. covers the entire C-band. The total absorption can be retained above 75% wide incident angle up to 600 under both and TM polarizations. The electric and current distributions at three distinct montion peaks are analyzed to explain the mechanism. Also, the physical manism, which is confirmed by the retrieved constitutive electromagnetic, is mainly contributed by the magnetic resonance. In addition, the proposed MA presents an excellent practical feasibility in term of compact structure (unit cell dimension of $\sim\!\!\lambda\!/6.5$ and thickness of $\sim\!\!\lambda\!/11.8$ at the center frequency) and wide incident angle insensitivity. The proposed MA in this work may find applications in the C-band defense and stealth systems that require only copolarization.

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